

NASA-CR-178,100

NASA Contractor Report 178100

ICASE REPORT NO. 86-20

NASA-CR-178100
19860016256

ICASE

THE CONSTRUCTION AND USE OF DIVERGENCE FREE
VECTOR EXPANSIONS FOR INCOMPRESSIBLE FLUID FLOW CALCULATIONS

Nessan Mac Giolla Mhuiris

FOR INFORMATION

STANDARD INFORMATION

LIBRARY COPY

Contract No. NAS1-17070

April 1986

JUN 19 1986

LANGLEY RESEARCH CENTER
LIBRARY, NASA
HAMPTON, VIRGINIA

INSTITUTE FOR COMPUTER APPLICATIONS IN SCIENCE AND ENGINEERING
NASA Langley Research Center, Hampton, Virginia 23665

Operated by the Universities Space Research Association



National Aeronautics and
Space Administration

Langley Research Center
Hampton, Virginia 23665

ENTER:

DISPLAY 37/6/1

86N25728*# ISSUE 16 PAGE 2585 CATEGORY 34 RPT#: NASA-CR-178100

ICASE-86-20 NAS 1.26:178100 CNT#: NAS1-17070 86/04/00 22 PAGES

UNCLASSIFIED DOCUMENT

UTTL: The construction and use of divergence free vector expansions for
incompressible fluid flow calculations TLSP: Final Report

AUTH: A/MHUIRIS, N. M. G.

CORP: National Aeronautics and Space Administration. Langley Research Center,
Hampton, Va. AVAIL. NTIS

SAP: HC A02/MF A01

CIO: UNITED STATES Submitted for publication

MAJS: /*APPROXIMATION/*CONSERVATION LAWS/*DIFFERENTIAL EQUATIONS/*EULER
EQUATIONS OF MOTION/*FLUID FLOW/*INCOMPRESSIBLE FLOW

MINS: / EXPANSION/ HYDRODYNAMICS/ NAVIER-STOKES EQUATION/ POLYNOMIALS

ABA: Author



The Construction and Use of Divergence Free Vector Expansions for Incompressible Fluid Flow Calculations

Nessan Mac Giolla Mhuiris

Institute for Computer Applications in Science and Engineering,
Mail Stop 132C, NASA Langley Research Center,
Hampton, Virginia 23665, USA.

ABSTRACT

For incompressible fluids the law of mass conservation reduces to a constraint on the velocity vector, namely that it be divergence free. This constraint has long been a source of great difficulty to the numericist seeking to discretize the Navier-Stokes and Euler equations. In this paper we will discuss a spectral method which overcomes this difficulty and we will demonstrate its efficacy on some simple problems. The velocity is approximated by a finite sum of divergence free vectors, each of which satisfies the same boundary conditions as the velocity. Projecting the governing equations onto the space of inviscid vector fields eliminates the pressure term and produces a set of ordinary differential equations that must be solved for the coefficients in the velocity sum. The pressure can then be recovered if it is needed.

The research for the author was supported in part by NSF Grant 830713 and by the National Aeronautics and Space Administration under NASA Contract No. NAS1 - 17070 while he was in residence at ICASE, NASA Langley Research Center, Hampton, VA 23665-5225.

1. Introduction.

We will be interested in the flow of incompressible fluids for which the physical law of mass conservation reduces to a constraint on the velocity vector of the fluid, namely that it be divergence free. The pressure in such flows is not then a thermodynamic variable determined by an equation of state but rather can be thought of as a Lagrange multiplier which adjusts itself instantaneously to ensure that this kinematical constraint on the velocity vector is satisfied. There is no evolution equation for the pressure nor does it satisfy any predetermined boundary or initial conditions.

Numericists, seeking to solve the governing equations approximately, have found that their greatest difficulty lies in the treatment of the pressure variable. While many ingenious methods have been devised to overcome the difficulties, the treatment advocated in this work is in a mathematical sense the most natural and offers many computational advantages. Here, the pressure term is eliminated from the equations entirely, and the divergence free condition is satisfied exactly by the numerically obtained approximation to the velocity vector. Moreover, as the components of the velocity are expanded in terms of series of polynomials which are solutions of a singular Sturm Liouville problem, whose excellent approximation properties are well documented, (e.g., Gottlieb & Orszag [1977], Quarteroni [1983]) convergence of our approximation will be bound only by the smoothness of the solution and by the number of terms used in the component expansions. For infinitely differentiable velocity fields we should expect to achieve "exponential convergence" (Canuto et al.) .

The essence of the method involves expanding the velocity in a series of divergence free vector fields each of which satisfies the same boundary conditions as the velocity and where in general the coefficients in the expansion are time dependent. The infinite sums are truncated and

substituted into the governing equations, which are the Navier-Stokes or Euler equations. Inner products are taken with vectors fields that satisfy inviscid boundary conditions, eliminating the pressure term and giving rise to a set of coupled ordinary differential equations for the coefficients. Nonlinear terms are treated explicitly in the time marching scheme, but the linear viscous terms can be treated implicitly. The method can also be used to solve linear stability problems; for these we will get a generalized matrix eigenvalue problem rather than a set of ordinary differential equations. The eigenvalue determines the stability of the base flow and each eigenfunction is the set of coefficients in the expansion of the corresponding perturbation velocity field.

In the next section of this paper we will see how to construct complete sets of solenoidal vector fields assuming that these are periodic in two directions. There have been various applications of the method both to simulate certain fluid flows (e.g., Moser & Moin's [1984] work on the infinite Taylor-Couette system) and also to solve linear stability problems for rather complex base flows (Mac Giolla Mhuiris [1986]). For pedagogical purposes, in this short paper we will consider the linear stability of a rotating Poiseuille flow. Extensive applications of the method to a set of more taxing stability problems that arise in the context of a fluid flow phenomenon known as vortex breakdown will be published elsewhere. We will also indicate how the method was used to simulate the infinite Taylor-Couette system.

2. Divergence Free Vector Bases.

It is well known (Ladyshenskaya [1966]) that the space of square integrable vector functions, $L^2(D)$ defined on a bounded domain D ($D \subset R^n$, $n = 2,3$) can be decomposed into those that are divergence free and whose normal components vanish on the boundary and those that can be expressed as the gradient of a differentiable function defined on D . The domains of interest for

this paper are either cylindrical or annular. For now we will consider vector fields defined on the section of a cylinder, T which are periodic in both the axial and azimuthal variables, having as their axial period the tube length, $2H$.

We will decompose $L^2(T)$ as follows.

$$L^2(T) = J(T) + J^\perp(T), \quad (2.1)$$

where,

$$J(T) = \left\{ \begin{array}{l} (a) \nabla \cdot \underline{u} = 0 \text{ in } T, \\ \underline{u} \in L^2(T) \quad (b) \underline{u} \cdot \underline{n} = 0 \text{ on } \partial T, \\ (c) \underline{u}|_{S_1} = \underline{u}|_{S_2}. \end{array} \right\} \quad (2.2)$$

S_1 and S_2 represent the ends of the cylinder. Given in this form $J(T)$ is clearly the space of

(a) incompressible, (b) inviscid, (c) periodic velocity fields.

The set of "viscous" velocity fields on T is a subset of $J(T)$ denoted $J^0(T)$.

$$J^0(T) = \left\{ \underline{u} \in J(T) \mid \underline{u} = 0 \text{ on } \partial T \right\}. \quad (2.3)$$

An alternative representation of $J(T)$ (Richtmyer [1978]) is given by,

$$J(T) = \left\{ \begin{array}{l} (a) \langle \underline{u}, \nabla p \rangle = 0 \text{ for all } p \in C^\infty(\overline{T}) \\ \underline{u} \in L^2(T) \\ (b) \underline{u}|_{S_1} = \underline{u}|_{S_2} \end{array} \right\} \quad (2.4)$$

where \overline{T} is the closure of T and $\langle \cdot, \cdot \rangle$ represents the usual inner product in $L^2(T)$,

$$\langle \underline{u}, \underline{v} \rangle = \int_T \underline{u} \cdot \underline{v} \, r dr d\theta dz. \quad (2.5)$$

The space $J(T)$ endowed with this inner product is a Hilbert space and a closed subspace of

$L^2(T)$.

The projection of $L^2(T)$ onto $J(T)$ will be denoted by Π . It is clear that vectors of the form ∇p are perpendicular to all \underline{u} in $J(T)$ and in fact (Ladyshenskaya [1966]),

$$J^1(T) = \left\{ \underline{u} \in L^2(T) \mid \underline{u} = \nabla p \text{ for some } p \text{ in } C^1(\overline{T}) \right\}. \quad (2.6)$$

Π then has the following properties,

$$\Pi : L^2(T) \rightarrow J(T), \quad (2.7)$$

$$\Pi \underline{u} = \underline{u} \quad \text{for all } \underline{u} \in J(T), \quad (2.8)$$

$$\Pi \nabla p = 0 \quad \text{for all } p \in C^1(\overline{T}). \quad (2.9)$$

To solve the Navier-Stokes equations in the domain T with periodic boundary conditions in the axial and azimuthal directions, we seek a vector \underline{u} in $J^0(T)$ satisfying,

$$\underline{u}_t + (\underline{u} \cdot \nabla) \underline{u} = -\nabla p + \nu \nabla^2 \underline{u}, \quad (2.10)$$

where ν is the kinematic viscosity of the fluid.

We can eliminate the ∇p term in this equation by means of the projection Π and, using some vector identities, we arrive at the following equation for \underline{u} .

$$\underline{u}_t = \Pi \left\{ \underline{\omega} \times \underline{u} - \nu \nabla \times \underline{\omega} \right\} \quad (2.11)$$

where $\underline{\omega}$ is the vorticity, $\underline{\omega} = \nabla \times \underline{u}$.

Projection of the Navier-Stokes equation onto a finite dimensional subspace, $J_N(T)$ of $J(T)$ is achieved in practice by taking the inner product of the equation with basis vectors for $J_N(T)$. This process eliminates the operator Π from the equation, for given any vector \underline{f} in $L^2(T)$ and

any vector $\underline{\Delta}$ in $J(T)$ we have that,

$$\langle \Pi \underline{f}, \underline{\Delta} \rangle = \langle \underline{f}, \underline{\Delta} \rangle, \quad (2.12)$$

as projections are self adjoint and as the projection of any vector in $J(T)$ is itself.

It is worth emphasizing that although we are solving the equations for a viscous fluid we nevertheless project the governing equations onto the space of inviscid vector fields. The reason for this is that having found a velocity \underline{u} such that the vector \underline{f} defined as,

$$\underline{f} = \underline{u}_t - \underline{\omega} \times \underline{u} + \nu \nabla \times \underline{\omega} \quad (2.13)$$

is orthogonal to all $\underline{\Delta}$ in $J(T)$ then $\underline{f} \in J^\perp(T)$ and so there exists a scalar function p (a pressure) with $\underline{f} = \nabla p$. If, however, \underline{f} were in $J^{0\perp}(T)$, which contains $J^\perp(T)$, the existence of a pressure is not guaranteed; consequently, \underline{u} may not correspond to a physical solution.

Leonard and Wray [1982] demonstrated a divergence free vector function expansion on a cylindrical domain for viscous velocity fields that are Fourier decomposable in both the axial and azimuthal variables. Mac Giolla Mhuiris [1986] considered expansions in terms of somewhat different basis functions, and it is these which will be described here.

The velocity field, \underline{u} , satisfies the continuity equation and is Fourier decomposable in z and θ , which means in effect that only two of its three components, u, v, w are independent. This motivates the introduction of two vector families, $\underline{\chi}_n^\pm$ in an expansion of the form,

$$\underline{u} = \sum_{nkm} \left\{ a_{2nkm}(t) \underline{\chi}_n^+(r) + a_{2n-1km}(t) \underline{\chi}_n^-(r) \right\} e^{i(kz + m\theta)}. \quad (2.14)$$

The components of the vectors $\underline{\chi}_n^\pm$ are found as follows. Expand two of the velocity components, say the first and the third, independently as,

$$u = \sum_{nkm} a_{2n-1km}(t) f_n^-(r) e^{i(kz + m\theta)}, \quad (2.15)$$

$$w = \sum_{nkm} a_{2nkm}(t) f_n^+(r) e^{i(kz + m\theta)}, \quad (2.16)$$

where $f_n^\pm(r)$ are complete sets of polynomials chosen to satisfy the boundary conditions that are imposed on u, w . The r and z components of $\underline{\chi}_n^\pm$ have now been picked, and it remains for us to choose the θ components in a manner that ensures the vectors $\underline{\chi}_n^\pm e^{i(kz + m\theta)}$ are divergence free. Consider for example, $\underline{\chi}_n^-(r)$.

$$\underline{\nabla} \cdot \left(\underline{\chi}_n^-(r) e^{i(kz + m\theta)} \right) = 0, \quad (2.17)$$

=>

$$(rf_n^-(r))' + im\chi_{n,\theta}^- = 0, \quad (2.18)$$

where the prime denotes a derivative with respect to r . This equation gives us the θ component of $\underline{\chi}_n^-(r)$. Rescaling, it is found that an expansion of the form (2.14) is possible for non-zero azimuthal wavenumbers where,

$$\underline{\chi}_n^-(r) = \left(imf_n^-(r), - (rf_n^-(r))', 0 \right), \quad (2.19)$$

$$\underline{\chi}_n^+(r) = \left(0, -rkf_n^+(r), mf_n^+(r) \right) \quad (2.20)$$

and such an expansion will guarantee that \underline{u} is divergence free. This expansion is clearly incomplete for azimuthal wave number zero, ($m = 0$), i.e., for axisymmetric flows and for that case the following expansion vectors can be used.

$$\underline{\chi}_n^-(r) = \left(ikf_n^-(r), 0, -\frac{1}{r} (rf_n^-(r))' \right), \quad (2.21)$$

$$\underline{\chi}_n^+(r) = \left(0, f_n^+(r), 0 \right). \quad (2.22)$$

The polynomials $f_n^\pm(r)$ must be chosen so that the vector \underline{u} given by (2.14) satisfies appropriate (viscous or inviscid) boundary conditions on the walls of the domain, T , and is single valued at the origin, $r = 0$. We will denote the polynomials used in the inviscid case by $a_n^\pm(r)$ reserving $f_n^\pm(r)$ for viscous expansions. We have then upon truncating (2.14) an approximation to \underline{u} of the form,

$$\underline{u}_{NKM} = \sum_{n=1}^N \sum_{k=-K}^K \sum_{m=-M}^M a_{nkm}(t) \underline{D}_{nkm}(r, z, \theta) \quad (2.23)$$

where,

$$\underline{D}_{nkm}(r, z, \theta) = \underline{\chi}_n^\pm(r; k, m) e^{i(kz + m\theta)}. \quad (2.24)$$

The projection vectors will have the same form as the expansion vectors, i.e., we will project with vectors, $\underline{\Delta}_{lpq}(r, z, \theta)$, where

$$\underline{\Delta}_{lpq}(r, z, \theta) = \underline{\xi}_l^\pm(r; k, m) e^{i(pz + q\theta)} \quad (2.25)$$

for

$$l = 1, \dots, N; \quad p = -K, \dots, K; \quad q = -M, \dots, M$$

with the vectors $\underline{\xi}_l^\pm$ being given by equations (2.19 - 22) using the inviscid polynomials, $a_l^\pm(r)$ for the components.

It is possible to choose the polynomials $a_l^\pm(r)$ and $f_n^\pm(r)$ in many different ways. Leonard & Wray [1982] in their consideration of certain turbulence simulations employed an unusual class of Jacobi polynomials to reduce the bandwidth of the final matrix system. These polynomials were also used by Spalart [1983] in his simulations of boundary-layer transition. Moser & Moin [1984], in their work on the infinite Taylor-Couette system, used Tchebychev polynomials and incorporated the weight function, against which these polynomials are orthogonal, into the projection

vectors. Mac Giolla Mhuiris [1986], investigating the temporal stability of a set of flows that are said to model vortex breakdown, (Leibovich [1984]) experimented with various sets of polynomials and found that Legendre polynomials were, perhaps, the easiest to use. All of the above sets are solutions to singular Sturm Liouville problems, and consequently we can expect expansions in terms of any of these polynomials to exhibit excellent convergence properties.

The single valuedness criterion, which must be applied along the center line of the tube for the vector \underline{u} , causes the polynomials $f_n^\pm(r)$ and $a_l^\pm(r)$ to depend on m , the azimuthal wavenumber (Joseph [1970]). One appropriate choice for $a_l^\pm(r)$ in the case of pipe flow is,

$$\begin{aligned} a_l^+(r) &= rP_l(2r-1) && \text{for all } m, \\ a_l^-(r) &= (1-r)P_l(2r-1) && \text{if } |m| = 1, \\ a_l^-(r) &= r(1-r)P_l(2r-1) && \text{if } |m| \neq 1, \end{aligned} \tag{2.26}$$

where the radial variable has been scaled by the tube radius and $P_l(r)$ is the Legendre polynomial of order l (Abramowitz & Stegun [1970]). The corresponding choice for $f_n^\pm(r)$ is,

$$\begin{aligned} f_n^+(r) &= r(1-r)P_n(2r-1) && \text{for all } m, \\ f_n^-(r) &= (1-r)^2P_n(2r-1) && \text{if } |m| = 1, \\ f_n^-(r) &= r(1-r)^2P_n(2r-1) && \text{if } |m| \neq 1. \end{aligned} \tag{2.27}$$

For the problems tackled to date, all of which separate in some sense in the azimuthal direction, this dependence on m presents no difficulty. We solve separate problems for each azimuthal wavenumber; so having chosen an m the expansion and projection sets are fixed throughout the calculation. Indeed, in theory there is no difficulty even if the problem at hand is truly three dimensional; however, some care is required in implementing the method to ensure that the

correct radial polynomial set is being used for each azimuthal component of the velocity.

3. Linear Stability Problems.

To determine the linear stability of a solution \underline{U} of, say, the Navier-Stokes equations, we consider whether infinitesimal perturbations to that solution grow in time. Therefore we linearize the governing equations about \underline{U} and seek solutions of the form,

$$\underline{u}(r, z, \theta) e^{-i\sigma t}. \quad (3.1)$$

The character of σ then determines the linear temporal stability of \underline{U} . If $\sigma = \alpha + i\beta$ where α, β are real, then

$$\begin{aligned} \beta > 0 & \Rightarrow \underline{U} \text{ is unstable} \\ \beta = 0 & \Rightarrow \underline{U} \text{ is neutrally stable} \\ \beta < 0 & \Rightarrow \underline{U} \text{ is stable.} \end{aligned} \quad (3.2)$$

The equations that must be solved have the form,

$$i\sigma \underline{u} = E\underline{u} + \text{Re}^{-1} S\underline{u}. \quad (3.3)$$

E and S are operators defined on $J(T)$ as follows,

$$S\underline{u} = -\Pi(\underline{\nabla} \times \underline{\omega}) \quad (3.5)$$

and

$$E\underline{u} = \Pi(\underline{\omega} \times \underline{U} + \underline{\Omega} \times \underline{u}), \quad (3.6)$$

where $\underline{\Omega}$ is the base flow vorticity, $\underline{\Omega} = \underline{\nabla} \times \underline{U}$. Some suitable nondimensionalization has introduced the Reynolds number,

$$\text{Re} = \frac{U_0 R_0}{\nu}, \quad (3.4)$$

R_0 and U_0 being characteristic length and velocity scales associated with the base flow. We can take R_0 to be the radius of the tube and U_0 to be the maximum value of the base flow azimuthal velocity.

We will solve (3.3) approximately by using the expansion \underline{u}_{NKM} for \underline{u} , taking inner products with the projection vectors, $\underline{\Delta}_{pq}$ and solving the resulting generalized matrix eigen problem for the eigenvalues σ and the eigenvectors a_{nkm} . (In this case, of course, these coefficients do not depend on time.) In general this matrix problem can be written as,

$$\sigma \bar{A} a = \left(\bar{B} + \frac{i}{\text{Re}} \bar{C} \right) a. \quad (3.7)$$

The matrix \bar{A} is purely real and arises from the fact that the expansion and projection vectors are not orthogonal.

$$\bar{A}_{lnpkqm} = \langle \underline{\Delta}_{pq}, \underline{D}_{nkm} \rangle, = \langle \underline{\xi}_l, \underline{x}_n \rangle \delta_{pk} \delta_{qm}, \equiv A_{ln} \delta_{pk} \delta_{qm}, \quad (3.8)$$

The Kronecker delta symbol, δ_{ij} arises because the Fourier bases employed in the axial and azimuthal directions are orthogonal. The matrix \bar{B} arising from the convection terms is also purely real.

$$\bar{B}_{lnpkqm} = \langle \underline{\Delta}_{pq}, (\underline{\nabla} \times \underline{D}_{nkm}) \times \underline{U} + \underline{\Omega} \times \underline{D}_{nkm} \rangle. \quad (3.9)$$

Finally, the matrix \bar{C} arising from the viscous terms is purely imaginary.

$$\bar{C}_{lnpkqm} = \langle \underline{\Delta}_{pq}, \underline{\nabla} \times \underline{\nabla} \times \underline{D}_{nkm} \rangle. \quad (3.10)$$

Using the orthogonality of the Fourier bases, it can be written as,

$$\overline{C}_{lnpkqm} = C_{ln} \delta_{pk} \delta_{qm}. \quad (3.11)$$

The form of the matrix \overline{B} depends on the base flow \underline{U} . If \underline{U} is independent of z and θ then it will be possible to find a matrix B such that,

$$\overline{B}_{lnpkqm} = B_{ln} \delta_{pk} \delta_{qm}. \quad (3.12)$$

This simply corresponds to the fact that the partial differential equation (3.3) separates in z and θ , for base flows that are independent of those variables. The stability of such flows can be determined by solving the $N \times N$ generalized matrix eigen problem,

$$\sigma A a = \left(B + \frac{i}{\text{Re}} C \right) a. \quad (3.13)$$

The matrices A , B , and C all depend parametrically on the wavenumbers of the projection and expansion vectors so it is advisable to separate them into submatrices that can be evaluated independently of these and any other parameters occurring in the base flow. The submatrices are evaluated once and then stored in the computer. The required integrations can be done at very little cost by utilizing the orthogonality properties of the expansion and projection polynomials. The full matrices can then be reassembled without the need for doing any further integrations.

One can always band the A and C matrices by appropriate choice of the polynomials $f_n^\pm(r)$ and $a_i^\pm(r)$. However the matrix B will generally be full, though for certain rather simple base flows such as the Hagen Poiseuille flow considered by Leonard & Wray [1982] it is also possible to band B . It is also worth noting that the matrix problem we get when considering the inviscid stability of base flows is a purely real one, and consequently the eigenvalues occur, as they should do, in conjugate pairs.

To demonstrate the method let us consider the viscous stability of a rotating Poiseuille flow,

$$\underline{U} = \left(0, V_0 r, (1 - r^2) \right). \quad (3.14)$$

Cotton et al. [1980] found that this flow with $V_0 = 0.2147$ was neutrally stable to disturbances having azimuthal wavenumber, $m = 1$ and axial wavenumber, $k = -1$. The following table lists the most unstable eigenvalue found for this flow using a code which implements the method we have discussed in the previous section (with Legendre polynomials as the radial basis functions). The first column of the table gives N , the number of radial basis vectors that were used to obtain the eigenvalue given in the next two columns; N is also the order of the matrix problem that needs to be solved at each step.

| Most unstable eigenvalue found for the rotating Poiseuille flow (3.14) with $m = 1$, $k = -1$, and $V_0 = 0.2147$. | | |
|--|--------------|-------------|
| N | frequency | growth rate |
| 4 | -0.00029 | .00334 |
| 6 | -0.00279 | .00101 |
| 10 | -0.00284 | .000001 |
| 14 | -0.002847 | .0000001 |
| 18 | -0.002847898 | .0000001379 |
| 22 | -0.002847898 | .0000001378 |

The convergence is exponential in N or some power of N , and there is no evidence of significant roundoff error.

We also used the divergence free expansion method to solve the adjoint stability problem which can be written as follows,

$$i\lambda \underline{u} = E^* \underline{u} + \frac{1}{\text{Re}} S \underline{u}. \quad (3.15)$$

The operator E^* is the adjoint operator to E and is given by,

$$E^* \underline{u} = -\Pi \left(\underline{\Omega} \times \underline{u} + \underline{\nabla} \times (\underline{u} \times \underline{U}) \right). \quad (3.16)$$

The direct and adjoint spectra obtained by solving (3.3) and (3.15) should, of course, be conjugate to each other, and how well a numerical scheme reproduces this theoretical result is a test of its accuracy. The following table lists the corresponding adjoint eigenvalue found by solving (3.15) for the base flow and wavenumber pair considered previously.

| Eigenvalue found by doing the adjoint problem (3.15) for the flow (3.13), with $m = 1$, $k = -1$, and $V_0 = 0.2147$. | | |
|---|--------------|--------------|
| N | frequency | growth rate |
| 4 | -0.00270 | -.000094 |
| 6 | -0.00280 | -.000013 |
| 10 | -0.00284 | -.000004 |
| 14 | -0.002847 | -.0000002 |
| 18 | -0.002847898 | -.0000001379 |
| 22 | -0.002847898 | -.0000001379 |

Clearly the agreement between the adjoint and direct results is excellent.

4. Flow Simulations

The global nature of the expansion functions we are considering here causes them to be extremely inefficient for the direct evaluation of nonlinearities such as the convective derivative term that occurs in the Navier-Stokes and Euler equations. However it is possible to use the so-called collocation technique (see for example Orszag [1972] or Kreiss & Oliger [1971]) in conjunction with our divergence free expansions to alleviate this problem.

The idea is to evaluate the nonlinear terms in physical space, expressing the result of this calculation (a vector function known on a set of grid points), componentwise, as a series of the

selected basis polynomials being used to form the projection vectors. The orthogonality properties of these polynomials can then be used to evaluate the needed inner products efficiently. The term $\langle \underline{\omega}_N \times \underline{u}_N, \underline{\Delta} \rangle$ is evaluated as follows, where for simplicity we assume that the terms are functions of just a single variable, r .

(1) Evaluate \underline{u}_N at the collocation points, $r_i, i = 1, \dots, N$.

(2) Evaluate $\underline{\omega}_N$ there also.

(The derivatives of \underline{u}_N are evaluated spectrally.)

(3) Evaluate $\underline{f}_N \equiv \underline{\omega}_N \times \underline{u}_N$ at the collocation points.

(4) Express each component of \underline{f}_N as a series of the appropriate polynomials.

(5) Evaluate the integrals $\langle \underline{f}_N, \underline{\Delta} \rangle$ utilizing the orthogonality properties of these polynomials.

When using Tchebychev polynomials to form the expansion and projection vectors, the transformations needed in step (4) can be very efficiently carried out (in $O(N \log N)$ operations) by means of Fast Fourier Transforms (see, for example, (Canuto et al.)); however, it is then important to include the weight function, $(1 - r^2)^{-\frac{1}{2}}$ (assuming $r \in [-1, 1]$), in the definition of the projection vectors so that we can carry out step (5) efficiently (Moser & Moin [1984]). We also mention in passing that to avoid aliasing errors it is necessary to use more collocation points than the number of modes, N , in the expansion.

For the time discretization scheme, the viscous terms are generally advanced by means of the trapezoidal rule (Crank-Nicholson) with an Adams-Bashforth scheme being used for the non-linear term, \underline{f} . Such a scheme is indicated in the following equation where the superscript denotes

the time level and δt is the step size being used:

$$\frac{u^{j+1}-u^j}{\delta t} = \frac{1}{2} \left(3\underline{f}^j - \underline{f}^{j-1} \right) - \frac{1}{2Re} \left(\underline{\nabla} \times \underline{\omega}^{j+1} + \underline{\nabla} \times \underline{\omega}^j \right). \quad (4.1)$$

The velocity is represented by a truncated expansion, \underline{u}_{NKL} with the coefficients now depending on the time, t . Projections are taken with vectors $\underline{\Delta}_{pq}$ to get the following set of linear equations to solve for the coefficients, a at the new time level, $j+1$:

$$\left(A - \frac{\delta t}{2Re} C \right) a^{j+1} = \left(A + \frac{\delta t}{2Re} C \right) a^j + \frac{\delta t}{2} \left(3F^j - F^{j-1} \right), \quad (4.2)$$

where C and A are essentially the same matrices we had before arising respectively from the viscous terms and the non-orthogonality of the expansion and projection vectors terms while F represents the projection of \underline{f} ,

$$F \equiv \langle \underline{f}, \underline{\Delta} \rangle. \quad (4.3)$$

Moser & Moin [1984] used a similar scheme to compute several states of the infinite Taylor-Couette flow successfully and went on to simulate turbulent flow in a mildly curved channel. For example, using just nine Fourier modes in the z direction and eleven Tchebychev polynomials in the r direction they found that the critical Reynolds number for transition to Taylor vortices was at $Re = 185$ for cylinders with an inner to outer ratio, $\eta = 0.95$ and at $Re = 68.2$ when $\eta = 0.5$. These figures are in excellent agreement with the analysis of DiPrima & Eagles [1977] for both the narrow and wide gap problems. They also carried out a series of three dimensional Taylor-Couette flow calculations and had excellent agreement with experimental results for Reynolds numbers up to 1300 with $\eta = 0.877$ (for modulated wavy vortex flow) using thirty one Fourier modes in the z direction, fifteen in the θ direction, and thirty three Tchebychev polynomials in the radial directon.

5. Conclusions and Outlook

Divergence free expansions eliminate many of the problems that a numericist must face when discretizing the equations governing the flow of incompressible fluids. Use of such an expansion ensures that the computed velocity will be exactly solenoidal and also enforces all the necessary boundary conditions on that vector, including the no-slip condition on the solid boundaries. Projection with inviscid vectors eliminates the ∇p term from the governing equation and we can recover the pressure, if it is needed, once an adequately resolved velocity field has been obtained. Finally, as each component of the velocity is expressed as a sum of polynomials which are solutions to a singular Sturm Liouville problem, we can expect exponential convergence for a smooth \underline{u} .

There are some problems with this method also. In common with all global expansion methods it is not possible to consider complex physical domains directly -- these must be mapped onto some simpler configuration, which may not always be possible, or else split into simple subdomains, leaving us with the problem of connecting the solutions across the interfaces. This problem is by no means specific to the divergence free expansion technique but rather is inherent in all spectral methods. It must also be admitted that implementation of the vector expansions in a computer program is far from easy, requiring as it does, a significant amount of algebraic manipulation to subdivide the matrices that are used into submatrices that are independent of the parameters occurring in the problem. A symbolic language such as MACSYMA can be used to somewhat alleviate these latter difficulties.

Current research that utilizes divergence free expansions includes a simulation of the finite Taylor-Couette system with the aid of vectors that are aperiodic in both the radial and axial directions. We see this method as an excellent tool for the direct simulation of incompressible

flows, and it should have many applications in investigations of the fundamental problems of incompressible fluid mechanics.

6. Bibliography

- (1) Abramowitz, M. and Stegun, I., eds., 1970. *Handbook of Mathematical Functions with Formulas, Graphs and Mathematical Tables*. 10th ed. U.S. Gov. Printing Office.
- (2) Canuto, C., Hussaini, M.Y., Quarteroni, A. and Zang, T.A. (To appear). *Spectral Methods with Applications to Fluid Dynamics*. Springer-Verlag, New York.
- (3) DiPrima, R.C. and Eagles, P.M., 1977. Amplification rates and torques for Taylor-vortex flows between rotating cylinders. *Phys. Fluids* 20, 171.
- (4) Gottlieb, D. and Orszag, S., 1977. *Numerical Analysis of Spectral Methods: Theory and Applications*. *CBMS-NSF Regional Conference Series on Applied Mathematics*, Vol. 26. SIAM, Philadelphia.
- (5) Joseph, D.D., 1970. *Stability of Fluid Motions: Volume I*. *Springer Tracts in Natural Philosophy* Vol. 27, Springer-Verlag, New York.
- (6) Kreiss, H-O. and Oliger, J., 1971. Comparison of accurate methods for the integration of hyperbolic equations. *Report 36*. Dept. of Computer Science, Uppsala University, Sweden.
- (7) Ladyshenskaya, O. A., 1969. *The Mathematical Theory of Viscous Incompressible Flow*. Gordon and Breach, New York.
- (8) Leibovich, S., 1984. Vortex stability and breakdown: Survey and extension. *AIAA J.* 22, 1192.
- (9) Leonard, A. and Wray, A., 1982. A new numerical method for simulation of three dimensional flow in a pipe. *Proc. International Conference on Numerical Methods in Fluid Dynamics*, 8th, Aachen. *Lecture Notes in Physics*, Vol. 170 (ed. E. Krause). Springer-Verlag, New York, pp. 335-342.
- (10) Mac Giolla Mhuiris, N., 1986. *Numerical Calculations of the Stability of Some Axisymmetric Flows Proposed as a Model for Vortex Breakdown*. Ph.D. Dissertation, Cornell Univ.
- (11) Moser, R.D. and Moin, P., 1984. *Direct Numerical Simulation of Curved Turbulent Channel Flow*. NASA TM 85974.
- (12) Orszag, S.A., 1972. Numerical simulation of incompressible flows within simple boundaries: I. Galerkin (spectral) representation. *Studies in Applied Mathematics* 50, 293.
- (13) Quarteroni, A., 1983. Theoretical motivations underlying spectral methods. *Proc. Meeting INRIA - Novosibirsk*, Paris.

- (14) Richtmyer, R.D., 1978. *Principles of Advanced Mathematical Physics: Volume I. Texts and Monographs in Physics*, Springer-Verlag, New York.
- (15) Salwen, H., Cotton, F.W., and Grosch, C.E., 1980. Linear stability of Poiseuille flow in a circular pipe. *J. Fluid Mech.* 98, 273.
- (16) Spalart, P.R., 1983 Numerical simulation of boundary-layer transition. *Proc. International Conference on Numerical Methods in Fluid Dynamics*, 9th. *Lecture Notes in Physics*, Vol. 218 (ed. H. Araki), Springer-Verlag, New York, pp. 531-535.

| | | | | | |
|---|--|---|---|--|--|
| 1. Report No. NASA CR-178100 ICASE Report No. 86-20 | | 2. Government Accession No. | | 3. Recipient's Catalog No. | |
| 4. Title and Subtitle THE CONSTRUCTION AND USE OF DIVERGENCE FREE VECTOR EXPANSIONS FOR INCOMPRESSIBLE FLUID FLOW CALCULATIONS | | | | 5. Report Date April 1986 | |
| | | | | 6. Performing Organization Code | |
| 7. Author(s) Nessan Mac Giolla Mhuiris | | | | 8. Performing Organization Report No. 86-20 | |
| | | | | 10. Work Unit No. | |
| 9. Performing Organization Name and Address Institute for Computer Applications in Science and Engineering Mail Stop 132C, NASA Langley Research Center Hampton, VA 23665-5225 | | | | 11. Contract or Grant No. NAS1-17070 | |
| | | | | 13. Type of Report and Period Covered Contractor Report | |
| 12. Sponsoring Agency Name and Address National Aeronautics and Space Administration Washington, D.C. 20546 | | | | 14. Sponsoring Agency Code 505-31-83-01 | |
| | | | | | |
| 15. Supplementary Notes Langley Technical Monitor: Submitted to Proceedings of a J. C. South Spectral Methods Workshop Final Report | | | | | |
| 16. Abstract For incompressible fluids the law of mass conservation reduces to a constraint on the velocity vector, namely that it be divergence free. This constraint has long been a source of great difficulty to the numericist seeking to discretize the Navier-Stokes and Euler equations. In this paper we will discuss a spectral method which overcomes this difficulty and we will demonstrate its efficacy on some simple problems. The velocity is approximated by a finite sum of divergence free vectors, each of which satisfies the same boundary conditions as the velocity. Projecting the governing equations onto the space of inviscid vector fields eliminates the pressure term and produces a set of ordinary differential equations that must be solved for the coefficients in the velocity sum. The pressure can then be recovered if it is needed. | | | | | |
| 17. Key Words (Suggested by Authors(s)) incompressible fluid mechanics, spectral methods, hydrodynamic, stability divergence free expansion | | | 18. Distribution Statement 34 - Fluid Mechanics and Heat Transfer Unclassified - unlimited | | |
| 19. Security Classif.(of this report) Unclassified | | 20. Security Classif.(of this page) Unclassified | | 21. No. of Pages 21 | |
| | | | | 22. Price A02 | |

